

PROBLEM 5-10

Statement: Design a linkage to carry the body in Figure P5-1 through the three positions P_1, P_2 and P_3 at the angles shown in the figure. Use analytical synthesis without regard for the fixed pivots shown. Use the free choices given below.

Given: Coordinates of the points P_1 and P_2 with respect to P_1 :

$$P_{1x} := 0.0 \quad P_{1y} := 0.0 \quad P_{2x} := -1.236 \quad P_{2y} := 2.138$$

$$P_{3x} := -2.500 \quad P_{3y} := 2.931$$

Angles made by the body in positions 1, 2 and 3:

$$\theta_{P1} := 210 \cdot \text{deg} \quad \theta_{P2} := 147.5 \cdot \text{deg} \quad \theta_{P3} := 110.2 \cdot \text{deg}$$

Free choices for the **WZ** dyad :

$$\beta_2 := 30.0 \cdot \text{deg} \quad \beta_3 := 60.0 \cdot \text{deg}$$

Free choices for the **US** dyad :

$$\gamma_2 := -10.0 \cdot \text{deg} \quad \gamma_3 := 25.0 \cdot \text{deg}$$

Two argument inverse tangent $\text{atan2}(x, y) := \begin{cases} \text{return } 0.5 \cdot \pi & \text{if } x = 0 \wedge y > 0 \\ \text{return } 1.5 \cdot \pi & \text{if } x = 0 \wedge y < 0 \\ \text{return } \text{atan}\left(\left(\frac{y}{x}\right)\right) & \text{if } x > 0 \\ \text{atan}\left(\left(\frac{y}{x}\right)\right) + \pi & \text{otherwise} \end{cases}$

Solution: See Figure P5-1 and Mathcad file P0510.

1. Determine the magnitudes and orientation of the position difference vectors.

$$p_{21} := \sqrt{P_{2x}^2 + P_{2y}^2} \quad p_{21} = 2.470 \quad \delta_2 := \text{atan2}(P_{2x}, P_{2y}) \quad \delta_2 = 120.033 \text{ deg}$$

$$p_{31} := \sqrt{P_{3x}^2 + P_{3y}^2} \quad p_{31} = 3.852 \quad \delta_3 := \text{atan2}(P_{3x}, P_{3y}) \quad \delta_3 = 130.463 \text{ deg}$$

2. Determine the angle changes of the coupler between precision points.

$$\alpha_2 := \theta_{P2} - \theta_{P1} \quad \alpha_2 = -62.500 \text{ deg}$$

$$\alpha_3 := \theta_{P3} - \theta_{P1} \quad \alpha_3 = -99.800 \text{ deg}$$

3. Evaluate terms in the **WZ** coefficient matrix and constant vector from equations 5.26 and form the matrix and vector:

$$A := \cos(\beta_2) - 1 \quad B := \sin(\beta_2) \quad C := \cos(\alpha_2) - 1$$

$$D := \sin(\alpha_2) \quad E := p_{21} \cdot \cos(\delta_2) \quad F := \cos(\beta_3) - 1$$

$$G := \sin(\beta_3) \quad H := \cos(\alpha_3) - 1 \quad K := \sin(\alpha_3)$$

$$L := p_{31} \cdot \cos(\delta_3) \quad M := p_{21} \cdot \sin(\delta_2) \quad N := p_{31} \cdot \sin(\delta_3)$$

$$AA := \begin{pmatrix} A & -B & C & -D \\ F & -G & H & -K \\ B & A & D & C \\ G & F & K & H \end{pmatrix} \quad CC := \begin{pmatrix} E \\ L \\ M \\ N \end{pmatrix} \quad \begin{pmatrix} W_{Ix} \\ W_{Iy} \\ Z_{Ix} \\ Z_{Iy} \end{pmatrix} := AA^{-1} \cdot CC$$

The components of the **W** and **Z** vectors are:

$$\begin{aligned} W_{Ix} &= 2.920 & W_{Iy} &= 1.720 & Z_{Ix} &= -0.756 & Z_{Iy} &= -0.442 \\ \theta &:= \text{atan2}(W_{Ix}, W_{Iy}) & \theta &= 30.493 \text{ deg} & \phi &:= \text{atan2}(Z_{Ix}, Z_{Iy}) & \phi &= 210.303 \text{ deg} \end{aligned}$$

The length of link 2 is: $w := \sqrt{(W_{Ix}^2 + W_{Iy}^2)}$, $w = 3.389$

The length of vector **Z** is: $z := \sqrt{(Z_{Ix}^2 + Z_{Iy}^2)}$, $z = 0.876$

4. Evaluate terms in the **US** coefficient matrix and constant vector from equations 5.31 and form the matrix and vector:

$$\begin{aligned} A' &:= \cos(\gamma_2) - 1 & B' &:= \sin(\gamma_2) & C &:= \cos(\alpha_2) - 1 \\ D &:= \sin(\alpha_2) & E &:= p_{2I} \cdot \cos(\delta_2) & F' &:= \cos(\gamma_3) - 1 \\ G' &:= \sin(\gamma_3) & H &:= \cos(\alpha_3) - 1 & K &:= \sin(\alpha_3) \\ L &:= p_{3I} \cdot \cos(\delta_3) & M &:= p_{2I} \cdot \sin(\delta_2) & N &:= p_{3I} \cdot \sin(\delta_3) \end{aligned}$$

$$AA := \begin{pmatrix} A' & -B' & C & -D \\ F' & -G' & H & -K \\ B' & A' & D & C \\ G' & F' & K & H \end{pmatrix} \quad CC := \begin{pmatrix} E \\ L \\ M \\ N \end{pmatrix} \quad \begin{pmatrix} U_{Ix} \\ U_{Iy} \\ S_{Ix} \\ S_{Iy} \end{pmatrix} := AA^{-1} \cdot CC$$

The components of the **U** and **S** vectors are:

$$\begin{aligned} U_{Ix} &= -1.009 & U_{Iy} &= 2.693 & S_{Ix} &= -0.792 & S_{Iy} &= -2.418 \\ \sigma &:= \text{atan2}(U_{Ix}, U_{Iy}) & \sigma &= 110.545 \text{ deg} & \psi &:= \text{atan2}(S_{Ix}, S_{Iy}) & \psi &= 251.875 \text{ deg} \end{aligned}$$

The length of link 4 is: $u := \sqrt{(U_{Ix}^2 + U_{Iy}^2)}$, $u = 2.875$

The length of vector **S** is: $s := \sqrt{(S_{Ix}^2 + S_{Iy}^2)}$, $s = 2.544$

5. Solve for links 3 and 1 using the vector definitions of **V** and **G**.

$$\begin{aligned} \text{Link 3: } V_{Ix} &:= Z_{Ix} - S_{Ix} & V_{Ix} &= 0.036 \\ V_{Iy} &:= Z_{Iy} - S_{Iy} & V_{Iy} &= 1.976 \\ \theta_3 &:= \text{atan2}(V_{Ix}, V_{Iy}) & \theta_3 &= 88.968 \text{ deg} \end{aligned}$$

$$v := \sqrt{V_{Ix}^2 + V_{Iy}^2} \quad v = 1.977$$

Link 1: $G_{Ix} := W_{Ix} + V_{Ix} - U_{Ix} \quad G_{Ix} = 3.965$

$$G_{Iy} := W_{Iy} + V_{Iy} - U_{Iy} \quad G_{Iy} = 1.003$$

$$\theta_1 := \text{atan2}(G_{Ix}, G_{Iy}) \quad \theta_1 = 14.202 \text{ deg}$$

$$g := \sqrt{G_{Ix}^2 + G_{Iy}^2} \quad g = 4.090$$

6. Determine the initial and final values of the input crank with respect to the vector **G**.

$$\theta_{2i} := \theta - \theta_1 \quad \theta_{2i} = 16.291 \text{ deg}$$

$$\theta_{2f} := \theta_{2i} + \beta_3 \quad \theta_{2f} = 76.291 \text{ deg}$$

7. Define the coupler point with respect to point A and the vector **V**.

$$r_p := z \quad \delta_p := \phi - \theta_3$$

$$r_p = 0.876 \quad \delta_p = 121.335 \text{ deg}$$

8. Locate the fixed pivots in the global frame using the vector definitions in Figure 5-2.

$$O_{2x} := -z \cdot \cos(\phi) - w \cdot \cos(\theta) \quad O_{2x} = -2.164$$

$$O_{2y} := -z \cdot \sin(\phi) - w \cdot \sin(\theta) \quad O_{2y} = -1.278$$

$$O_{4x} := -s \cdot \cos(\psi) - u \cdot \cos(\sigma) \quad O_{4x} = 1.801$$

$$O_{4y} := -s \cdot \sin(\psi) - u \cdot \sin(\sigma) \quad O_{4y} = -0.274$$

9. Determine the rotation angle of the fourbar frame with respect to the global frame (angle from the global X axis to the line O_2O_4).

$$\theta_{rot} := \text{atan2}[(O_{4x} - O_{2x}), (O_{4y} - O_{2y})] \quad \theta_{rot} = 14.202 \text{ deg}$$

10. Determine the Grashof condition.

$$\text{Condition}(a, b, c, d) := \begin{cases} S \leftarrow \min(a, b, c, d) \\ L \leftarrow \max(a, b, c, d) \\ SL \leftarrow S + L \\ PQ \leftarrow a + b + c + d - SL \\ \text{return "Grashof" if } SL < PQ \\ \text{return "Special Grashof" if } SL = PQ \\ \text{return "non-Grashof" otherwise} \end{cases}$$

$$\text{Condition}(g, u, v, w) = \text{"Grashof"}$$

11. DESIGN SUMMARY

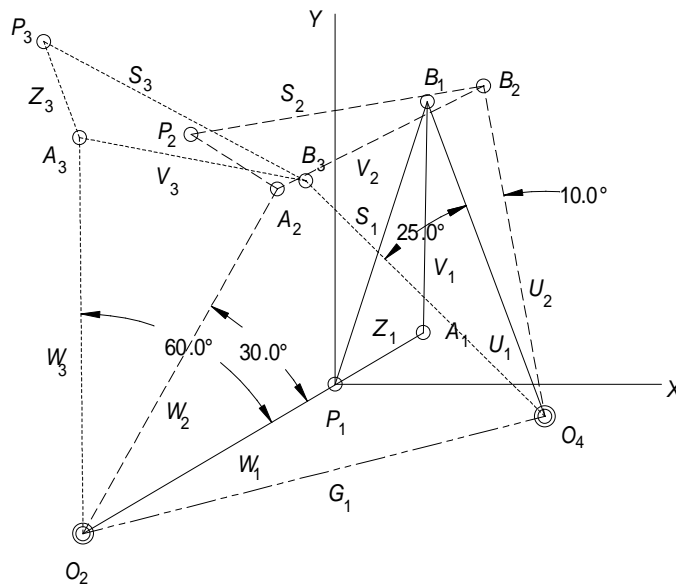
Link 2:	$w = 3.389$	$\theta = 30.493 \text{ deg}$
Link 3:	$v = 1.977$	$\theta_3 = 88.968 \text{ deg}$
Link 4:	$u = 2.875$	$\sigma = 110.545 \text{ deg}$
Link 1:	$g = 4.090$	$\theta_1 = 14.202 \text{ deg}$
Coupler:	$r_p = 0.876$	$\delta_p = 121.335 \text{ deg}$

Crank angles:

$$\theta_{2i} = 16.291 \text{ deg}$$

$$\theta_{2f} = 76.291 \text{ deg}$$

12. Draw the linkage, using the link lengths, fixed pivot positions, and angles above, to verify the design.



PROBLEM 5-12

Statement: Design a linkage to carry the body in Figure P5-2 through the two positions P_1 and P_2 at the angles shown in the figure. Use analytical synthesis without regard for the fixed pivots shown. Use the free choices given below.

Given: Coordinates of the points P_1 and P_2 with respect to P_1 :

$$P_{1x} := 0.0 \quad P_{1y} := 0.0 \quad P_{2x} := 1.903 \quad P_{2y} := 1.347$$

Angles made by the body in positions 1 and 2:

$$\theta_{P1} := 101.0 \text{ deg} \quad \theta_{P2} := 62.0 \text{ deg}$$

Free choices for the **WZ** dyad :

$$z := 2.000 \quad \beta_2 := 30.0 \text{ deg} \quad \phi := 150.0 \text{ deg}$$

Free choices for the **US** dyad :

$$s := 3.000 \quad \gamma_2 := 40.0 \text{ deg} \quad \psi := -50.0 \text{ deg}$$

Two argument inverse tangent

$$\text{atan2}(x, y) := \begin{cases} \text{return } 0.5 \cdot \pi & \text{if } x = 0 \wedge y > 0 \\ \text{return } 1.5 \cdot \pi & \text{if } x = 0 \wedge y < 0 \\ \text{return } \text{atan}\left(\left(\frac{y}{x}\right)\right) & \text{if } x > 0 \\ \text{atan}\left(\left(\frac{y}{x}\right)\right) + \pi & \text{otherwise} \end{cases}$$

Solution: See Figure P5-2 and Mathcad file P0512.

- Note that this is a two-position motion generation (MG) problem because the output is specified as a complex motion of the coupler, link 3. Because of the data given in the hint, the second method of Section 5.3 will be used here.
- Define the position vectors \mathbf{R}_1 and \mathbf{R}_2 and the vector \mathbf{P}_{21} using Figure 5-1 and equation 5.1.

$$\mathbf{R1} := \begin{pmatrix} P_{1x} \\ P_{1y} \end{pmatrix} \quad \mathbf{R2} := \begin{pmatrix} P_{2x} \\ P_{2y} \end{pmatrix} \quad \begin{pmatrix} P_{21x} \\ P_{21y} \end{pmatrix} := \mathbf{R2} - \mathbf{R1} \quad P_{21x} = 1.903$$

$$P_{21y} = 1.347$$

$$p_{21} := \sqrt{P_{21x}^2 + P_{21y}^2} \quad p_{21} = 2.331$$

- From the trigonometric relationships given in Figure 5-1, determine α_2 and δ_2 .

$$\alpha_2 := \theta_{P2} - \theta_{P1} \quad \alpha_2 = -39.000 \text{ deg}$$

$$\delta_2 := \text{atan2}(P_{21x}, P_{21y}) \quad \delta_2 = 35.292 \text{ deg}$$

- Solve for the **WZ** dyad using equations 5.8.

$$\begin{aligned} Z_{1x} &:= z \cdot \cos(\phi) & Z_{1x} &= -1.732 & Z_{1y} &:= z \cdot \sin(\phi) & Z_{1y} &= 1.000 \\ A &:= \cos(\beta_2) - 1 & A &= -0.134 & D &:= \sin(\alpha_2) & D &= -0.629 \end{aligned}$$

$$\begin{aligned}
 B &:= \sin(\beta_2) & B &= 0.500 & E &:= p_{2l} \cdot \cos(\delta_2) & E &= 1.903 \\
 C &:= \cos(\alpha_2) - 1 & C &= -0.223 & F &:= p_{2l} \cdot \sin(\delta_2) & F &= 1.347 \\
 W_{Ix} &:= \frac{A \cdot (-C \cdot Z_{Ix} + D \cdot Z_{Iy} + E) + B \cdot (-C \cdot Z_{Iy} - D \cdot Z_{Ix} + F)}{-2 \cdot A} & W_{Ix} &= 0.452 \\
 W_{Iy} &:= \frac{A \cdot (-C \cdot Z_{Iy} - D \cdot Z_{Ix} + F) + B \cdot (C \cdot Z_{Ix} - D \cdot Z_{Iy} - E)}{-2 \cdot A} & W_{Iy} &= -1.896 \\
 w &:= \sqrt{W_{Ix}^2 + W_{Iy}^2} & w &= 1.949 \\
 \theta &:= \text{atan2}(W_{Ix}, W_{Iy}) & \theta &= -76.607 \text{ deg}
 \end{aligned}$$

5. Solve for the **US** dyad using equations 5.12.

$$\begin{aligned}
 S_{Ix} &:= s \cdot \cos(\psi) & S_{Ix} &= 1.928 & S_{Iy} &:= s \cdot \sin(\psi) & S_{Iy} &= -2.298 \\
 A &:= \cos(\gamma_2) - 1 & A &= -0.234 & D &:= \sin(\alpha_2) & D &= -0.629 \\
 B &:= \sin(\gamma_2) & B &= 0.643 & E &:= p_{2l} \cdot \cos(\delta_2) & E &= 1.903 \\
 C &:= \cos(\alpha_2) - 1 & C &= -0.223 & F &:= p_{2l} \cdot \sin(\delta_2) & F &= 1.347 \\
 U_{Ix} &:= \frac{A \cdot (-C \cdot S_{Ix} + D \cdot S_{Iy} + E) + B \cdot (-C \cdot S_{Iy} - D \cdot S_{Ix} + F)}{-2 \cdot A} & U_{Ix} &= 0.924 \\
 U_{Iy} &:= \frac{A \cdot (-C \cdot S_{Iy} - D \cdot S_{Ix} + F) + B \cdot (C \cdot S_{Ix} - D \cdot S_{Iy} - E)}{-2 \cdot A} & U_{Iy} &= -6.216 \\
 u &:= \sqrt{U_{Ix}^2 + U_{Iy}^2} & u &= 6.284 \\
 \sigma &:= \text{atan2}(U_{Ix}, U_{Iy}) & \sigma &= -81.540 \text{ deg}
 \end{aligned}$$

6. Solve for links 3 and 1 using the vector definitions of **V** and **G**.

$$\begin{aligned}
 \text{Link 3: } V_{Ix} &:= z \cdot \cos(\phi) - s \cdot \cos(\psi) & V_{Ix} &= -3.660 \\
 V_{Iy} &:= z \cdot \sin(\phi) - s \cdot \sin(\psi) & V_{Iy} &= 3.298 \\
 \theta_3 &:= \text{atan2}(V_{Ix}, V_{Iy}) & \theta_3 &= 137.980 \text{ deg} \\
 v &:= \sqrt{V_{Ix}^2 + V_{Iy}^2} & v &= 4.927 \\
 \text{Link 1: } G_{Ix} &:= w \cdot \cos(\theta) + v \cdot \cos(\theta_3) - u \cdot \cos(\sigma) & G_{Ix} &= -4.133 \\
 G_{Iy} &:= w \cdot \sin(\theta) + v \cdot \sin(\theta_3) - u \cdot \sin(\sigma) & G_{Iy} &= 7.617
 \end{aligned}$$

$$\theta_1 := \text{atan2}(G_{1x}, G_{1y}) \quad \theta_1 = 118.485 \text{ deg}$$

$$g := \sqrt{G_{1x}^2 + G_{1y}^2} \quad g = 8.667$$

7. Determine the initial and final values of the input crank with respect to the vector **G**.

$$\theta_{2i} := \theta - \theta_1 \quad \theta_{2i} = -195.092 \text{ deg}$$

$$\theta_{2f} := \theta_{2i} + \beta_2 \quad \theta_{2f} = -165.092 \text{ deg}$$

8. Define the coupler point with respect to point A and the vector **V**.

$$r_p := z \quad \delta_p := \phi - \theta_3$$

$$r_p = 2.000 \quad \delta_p = 12.020 \text{ deg}$$

9. Locate the fixed pivots in the global frame using the vector definitions in Figure 5-2.

$$\rho_1 := \text{atan2}(P_{1x}, P_{1y}) \quad \rho_1 = 180.000 \text{ deg}$$

$$R_I := \sqrt{P_{1x}^2 + P_{1y}^2} \quad R_I = 0.000$$

$$O_{2x} := R_I \cos(\rho_1) - z \cos(\phi) - w \cos(\theta) \quad O_{2x} = 1.281$$

$$O_{2y} := R_I \sin(\rho_1) - z \sin(\phi) - w \sin(\theta) \quad O_{2y} = 0.896$$

$$O_{4x} := R_I \cos(\rho_1) - s \cos(\psi) - u \cos(\sigma) \quad O_{4x} = -2.853$$

$$O_{4y} := R_I \sin(\rho_1) - s \sin(\psi) - u \sin(\sigma) \quad O_{4y} = 8.514$$

10. Determine the rotation angle of the fourbar frame with respect to the global frame (angle from the global X axis to the line O_2O_4).

$$\theta_{rot} := \text{atan2}[(O_{4x} - O_{2x}), (O_{4y} - O_{2y})] \quad \theta_{rot} = 118.485 \text{ deg}$$

11. Determine the Grashof condition.

$$\text{Condition}(a, b, c, d) := \begin{cases} S \leftarrow \min(a, b, c, d) \\ L \leftarrow \max(a, b, c, d) \\ SL \leftarrow S + L \\ PQ \leftarrow a + b + c + d - SL \\ \text{return "Grashof" if } SL < PQ \\ \text{return "Special Grashof" if } SL = PQ \\ \text{return "non-Grashof" otherwise} \end{cases}$$

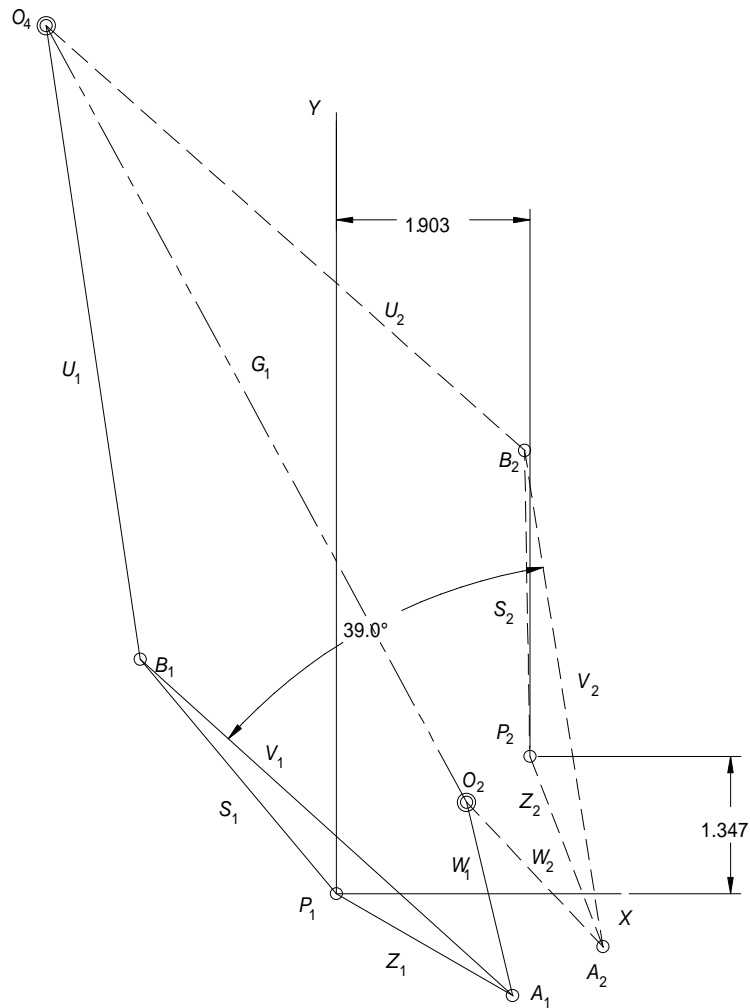
$$\text{Condition}(g, u, v, w) = \text{"Grashof"}$$

12. DESIGN SUMMARY

Link 2:	$w = 1.949$	$\theta = -76.607 \text{ deg}$
Link 3:	$v = 4.927$	$\theta_3 = 137.980 \text{ deg}$

Link 4: $u = 6.284$ $\sigma = -81.540 \text{ deg}$
 Link 1: $g = 8.667$ $\theta_1 = 118.485 \text{ deg}$
 Coupler: $r_p = 2.000$ $\delta_p = 12.020 \text{ deg}$
 Crank angles:
 $\theta_{2i} = -195.092 \text{ deg}$
 $\theta_{2f} = -165.092 \text{ deg}$

13. Draw the linkage, using the link lengths, fixed pivot positions, and angles above, to verify the design.



PROBLEM 5-15

Statement: Design a linkage to carry the body in Figure P5-2 through the three positions P_1, P_2 and P_3 at the angles shown in the figure. Use analytical synthesis and design it for the fixed pivots shown.

Given:

$P_{21x} := 1.903$	$P_{21y} := 1.347$	$P_{31x} := 1.389$	$P_{31y} := 1.830$
$O_{2x} := -0.884$	$O_{2y} := -1.251$	$O_{4x} := 3.062$	$O_{4y} := -1.251$
Body angles:	$\theta_{P1} := 101 \cdot \text{deg}$	$\theta_{P2} := 62 \cdot \text{deg}$	$\theta_{P3} := 39 \cdot \text{deg}$

Two argument inverse tangent $\text{atan2}(x, y) := \begin{cases} \text{return } 0.5 \cdot \pi & \text{if } x = 0 \wedge y > 0 \\ \text{return } 1.5 \cdot \pi & \text{if } x = 0 \wedge y < 0 \\ \text{return } \text{atan}\left(\left(\frac{y}{x}\right)\right) & \text{if } x > 0 \\ \text{atan}\left(\left(\frac{y}{x}\right)\right) + \pi & \text{otherwise} \end{cases}$

Solution: See Figure P5-2 and Mathcad file P0515.

1. Determine the angle changes between precision points from the body angles given.

$$\alpha_2 := \theta_{P2} - \theta_{P1} \qquad \alpha_2 = -39.000 \text{ deg}$$

$$\alpha_3 := \theta_{P3} - \theta_{P1} \qquad \alpha_3 = -62.000 \text{ deg}$$

2. Using Figure 5-6, determine the magnitudes of $\mathbf{R}_1, \mathbf{R}_2$, and \mathbf{R}_3 and their x and y components.

$$R_{1x} := -O_{2x} \qquad R_{1x} = 0.884 \qquad R_{1y} := -O_{2y} \qquad R_{1y} = 1.251$$

$$R_{2x} := R_{1x} + P_{21x} \qquad R_{2x} = 2.787$$

$$R_{2y} := R_{1y} + P_{21y} \qquad R_{2y} = 2.598$$

$$R_{3x} := R_{1x} + P_{31x} \qquad R_{3x} = 2.273$$

$$R_{3y} := R_{1y} + P_{31y} \qquad R_{3y} = 3.081$$

$$R_1 := \sqrt{R_{1x}^2 + R_{1y}^2} \qquad R_1 = 1.532$$

$$R_2 := \sqrt{R_{2x}^2 + R_{2y}^2} \qquad R_2 = 3.810$$

$$R_3 := \sqrt{R_{3x}^2 + R_{3y}^2} \qquad R_3 = 3.829$$

3. Using Figure 5-6, determine the angles that $\mathbf{R}_1, \mathbf{R}_2$, and \mathbf{R}_3 make with the x axis.

$$\zeta_1 := \text{atan2}(R_{1x}, R_{1y}) \qquad \zeta_1 = 54.754 \text{ deg}$$

$$\zeta_2 := \text{atan2}(R_{2x}, R_{2y}) \qquad \zeta_2 = 42.990 \text{ deg}$$

$$\zeta_3 := \text{atan2}(R_{3x}, R_{3y}) \qquad \zeta_3 = 53.582 \text{ deg}$$

4. Solve for β_2 and β_3 using equations 5.34

$$C_1 := R_3 \cdot \cos(\alpha_2 + \zeta_3) - R_2 \cdot \cos(\alpha_3 + \zeta_2) \qquad C_1 = 0.103$$

$$\begin{aligned}
 C_2 &:= R_3 \cdot \sin(\alpha_2 + \zeta_3) - R_2 \cdot \sin(\alpha_3 + \zeta_2) & C_2 &= 2.205 \\
 C_3 &:= R_1 \cdot \cos(\alpha_3 + \zeta_1) - R_3 \cdot \cos(\zeta_3) & C_3 &= -0.753 \\
 C_4 &:= -R_1 \cdot \sin(\alpha_3 + \zeta_1) + R_3 \cdot \sin(\zeta_3) & C_4 &= 3.274 \\
 C_5 &:= R_1 \cdot \cos(\alpha_2 + \zeta_1) - R_2 \cdot \cos(\zeta_2) & C_5 &= -1.313 \\
 C_6 &:= -R_1 \cdot \sin(\alpha_2 + \zeta_1) + R_2 \cdot \sin(\zeta_2) & C_6 &= 2.182 \\
 A_1 &:= -C_3^2 - C_4^2 & A_1 &= -11.288 \\
 A_2 &:= C_3 C_6 - C_4 C_5 & A_2 &= 2.654 \\
 A_3 &:= -C_4 C_6 - C_3 C_5 & A_3 &= -8.134 \\
 A_4 &:= C_2 C_3 + C_1 C_4 & A_4 &= -1.324 \\
 A_5 &:= C_4 C_5 - C_3 C_6 & A_5 &= -2.654 \\
 A_6 &:= C_1 C_3 - C_2 C_4 & A_6 &= -7.297 \\
 K_1 &:= A_2 A_4 + A_3 A_6 & K_1 &= 55.842 \\
 K_2 &:= A_3 A_4 + A_5 A_6 & K_2 &= 30.136 \\
 K_3 &:= \frac{A_1^2 - A_2^2 - A_3^2 - A_4^2 - A_6^2}{2} & K_3 &= -0.392 \\
 \beta_{31} &:= 2 \cdot \operatorname{atan} \left(\frac{K_2 + \sqrt{K_1^2 + K_2^2 - K_3^2}}{K_1 + K_3} \right) & \beta_{31} &= 118.708 \text{ deg} \\
 \beta_{32} &:= 2 \cdot \operatorname{atan} \left(\frac{K_2 - \sqrt{K_1^2 + K_2^2 - K_3^2}}{K_1 + K_3} \right) & \beta_{32} &= -62.000 \text{ deg}
 \end{aligned}$$

The second value is the same as α_3 , so use the first value

$$\beta_3 := \beta_{31}$$

$$\begin{aligned}
 \beta_{21} &:= \operatorname{acos} \left(\frac{A_5 \cdot \sin(\beta_3) + A_3 \cdot \cos(\beta_3) + A_6}{A_1} \right) & \beta_{21} &= 59.564 \text{ deg} \\
 \beta_{22} &:= \operatorname{asin} \left(\frac{A_3 \cdot \sin(\beta_3) + A_2 \cdot \cos(\beta_3) + A_4}{A_1} \right) & \beta_{22} &= 59.564 \text{ deg}
 \end{aligned}$$

Since both values are the same,

$$\beta_2 := \beta_{21}$$

5. Repeat steps 2, 3, and 4 for the right-hand dyad to find γ_1 and γ_2 .

$$\begin{aligned}
 R_{1x} &:= -O_{4x} & R_{1x} &= -3.062 & R_{1y} &:= -O_{4y} & R_{1y} &= 1.251 \\
 R_{2x} &:= R_{1x} + P_{21x} & R_{2x} &= -1.159 \\
 R_{2y} &:= R_{1y} + P_{21y} & R_{2y} &= 2.598
 \end{aligned}$$

$$R_{3x} := R_{1x} + P_{31x} \quad R_{3x} = -1.673$$

$$R_{3y} := R_{1y} + P_{31y} \quad R_{3y} = 3.081$$

$$R_1 := \sqrt{R_{1x}^2 + R_{1y}^2} \quad R_1 = 3.308$$

$$R_2 := \sqrt{R_{2x}^2 + R_{2y}^2} \quad R_2 = 2.845$$

$$R_3 := \sqrt{R_{3x}^2 + R_{3y}^2} \quad R_3 = 3.506$$

6. Using Figure 5-6, determine the angles that \mathbf{R}_1 , \mathbf{R}_2 , and \mathbf{R}_3 make with the x axis.

$$\zeta_1 := \text{atan2}(R_{1x}, R_{1y}) \quad \zeta_1 = 157.777 \text{ deg}$$

$$\zeta_2 := \text{atan2}(R_{2x}, R_{2y}) \quad \zeta_2 = 114.042 \text{ deg}$$

$$\zeta_3 := \text{atan2}(R_{3x}, R_{3y}) \quad \zeta_3 = 118.502 \text{ deg}$$

7. Solve for γ_2 and γ_3 using equations 5.34

$$C_1 := R_3 \cdot \cos(\alpha_2 + \zeta_3) - R_2 \cdot \cos(\alpha_3 + \zeta_2) \quad C_1 = -1.111$$

$$C_2 := R_3 \cdot \sin(\alpha_2 + \zeta_3) - R_2 \cdot \sin(\alpha_3 + \zeta_2) \quad C_2 = 1.204$$

$$C_3 := R_1 \cdot \cos(\alpha_3 + \zeta_1) - R_3 \cdot \cos(\zeta_3) \quad C_3 = 1.340$$

$$C_4 := -R_1 \cdot \sin(\alpha_3 + \zeta_1) + R_3 \cdot \sin(\zeta_3) \quad C_4 = -0.210$$

$$C_5 := R_1 \cdot \cos(\alpha_2 + \zeta_1) - R_2 \cdot \cos(\zeta_2) \quad C_5 = -0.433$$

$$C_6 := -R_1 \cdot \sin(\alpha_2 + \zeta_1) + R_2 \cdot \sin(\zeta_2) \quad C_6 = -0.301$$

$$A_1 := -C_3^2 - C_4^2 \quad A_1 = -1.840$$

$$A_2 := C_3 C_6 - C_4 C_5 \quad A_2 = -0.495$$

$$A_3 := -C_4 C_6 - C_3 C_5 \quad A_3 = 0.517$$

$$A_4 := C_2 C_3 + C_1 C_4 \quad A_4 = 1.847$$

$$A_5 := C_4 C_5 - C_3 C_6 \quad A_5 = 0.495$$

$$A_6 := C_1 C_3 - C_2 C_4 \quad A_6 = -1.236$$

$$K_1 := A_2 A_4 + A_3 A_6 \quad K_1 = -1.553$$

$$K_2 := A_3 A_4 + A_5 A_6 \quad K_2 = 0.344$$

$$K_3 := \frac{A_1^2 - A_2^2 - A_3^2 - A_4^2 - A_6^2}{2} \quad K_3 = -1.033$$

$$\gamma_{31} := 2 \cdot \text{atan} \left(\frac{K_2 + \sqrt{K_1^2 + K_2^2 - K_3^2}}{K_1 + K_3} \right) \quad \gamma_{31} = -62.000 \text{ deg}$$

$$\gamma_{32} := 2 \cdot \operatorname{atan}\left(\frac{K_2 - \sqrt{K_1^2 + K_2^2 - K_3^2}}{K_1 + K_3}\right) \quad \gamma_{32} = 36.991 \text{ deg}$$

The first value is the same as α_3 , so use the second value

$$\gamma_3 := \gamma_{32}$$

$$\gamma_{21} := \operatorname{acos}\left(\frac{A_5 \cdot \sin(\gamma_3) + A_3 \cdot \cos(\gamma_3) + A_6}{A_1}\right) \quad \gamma_{21} = 73.415 \text{ deg}$$

$$\gamma_{22} := \operatorname{asin}\left(\frac{A_3 \cdot \sin(\gamma_3) + A_2 \cdot \cos(\gamma_3) + A_4}{A_1}\right) \quad \gamma_{22} = -73.415 \text{ deg}$$

Since γ_2 is not in the first quadrant ,

$$\gamma_2 := \gamma_{22}$$

8. Use the method of Section 5.7 to synthesize the linkage. Start by determining the magnitudes of the vectors \mathbf{P}_{21} and \mathbf{P}_{31} and their angles with respect to the X axis.

$$p_{21} := \sqrt{P_{21x}^2 + P_{21y}^2} \quad p_{21} = 2.331$$

$$\delta_2 := \operatorname{atan2}(P_{21x}, P_{21y}) \quad \delta_2 = 35.292 \text{ deg}$$

$$p_{31} := \sqrt{P_{31x}^2 + P_{31y}^2} \quad p_{31} = 2.297$$

$$\delta_3 := \operatorname{atan2}(P_{31x}, P_{31y}) \quad \delta_3 = 52.801 \text{ deg}$$

9. Evaluate terms in the **WZ** coefficient matrix and constant vector from equations (5.25) and form the matrix and vector:

$$A := \cos(\beta_2) - 1 \quad B := \sin(\beta_2) \quad C := \cos(\alpha_2) - 1$$

$$D := \sin(\alpha_2) \quad E := p_{21} \cdot \cos(\delta_2) \quad F := \cos(\beta_3) - 1$$

$$G := \sin(\beta_3) \quad H := \cos(\alpha_3) - 1 \quad K := \sin(\alpha_3)$$

$$L := p_{31} \cdot \cos(\delta_3) \quad M := p_{21} \cdot \sin(\delta_2) \quad N := p_{31} \cdot \sin(\delta_3)$$

$$AA := \begin{pmatrix} A & -B & C & -D \\ F & -G & H & -K \\ B & A & D & C \\ G & F & K & H \end{pmatrix} \quad CC := \begin{pmatrix} E \\ L \\ M \\ N \end{pmatrix} \quad \begin{pmatrix} W1x \\ W1y \\ Z1x \\ Z1y \end{pmatrix} := AA^{-1} \cdot CC$$

10. The components of the **W** and **Z** vectors are:

$$W1x = 1.262 \quad W1y = -1.109 \quad Z1x = -0.378 \quad Z1y = 2.360$$

11. The length of link 2 is: $w := \sqrt{W1x^2 + W1y^2} \quad w = 1.680$

12. Evaluate terms in the **US** coefficient matrix and constant vector from equations (5.25) and form the matrix and vector:

$$\begin{array}{lll}
 A' := \cos(\gamma_2) - 1 & B' := \sin(\gamma_2) & C := \cos(\alpha_2) - 1 \\
 D := \sin(\alpha_2) & E := p_{2I} \cdot \cos(\delta_2) & F' := \cos(\gamma_3) - 1 \\
 G' := \sin(\gamma_3) & H := \cos(\alpha_3) - 1 & K := \sin(\alpha_3) \\
 L := p_{3I} \cdot \cos(\delta_3) & M := p_{2I} \cdot \sin(\delta_2) & N := p_{3I} \cdot \sin(\delta_3)
 \end{array}$$

$$AA := \begin{pmatrix} A' & -B' & C & -D \\ F' & -G' & H & -K \\ B' & A' & D & C \\ G' & F' & K & H \end{pmatrix} \quad CC := \begin{pmatrix} E \\ L \\ M \\ N \end{pmatrix} \quad \begin{pmatrix} UIx \\ UIy \\ SIx \\ SIy \end{pmatrix} := AA^{-1} \cdot CC$$

13. The components of the **W** and **Z** vectors are:

$$UIx = -0.326 \quad UIy = 0.830 \quad SIx = -2.736 \quad SIy = 0.421$$

14. The length of link 4 is: $u := \sqrt{UIx^2 + UIy^2} \quad u = 0.892$

15. Solving for links 3 and 1 from equations 5.2a and 5.2b.

$$VIx := ZIx - SIx \quad VIx = 2.359$$

$$VIy := ZIy - SIy \quad VIy = 1.939$$

The length of link 3 is: $v := \sqrt{VIx^2 + VIy^2} \quad v = 3.054$

$$GIx := WIx + VIx - UIx \quad GIx = 3.946$$

$$GIy := WIy + VIy - UIy \quad GIy = -1.110 \times 10^{-15}$$

The length of link 1 is: $g := \sqrt{GIx^2 + GIy^2} \quad g = 3.946$

16. Check the location of the fixed pivots with respect to the global frame using the calculated vectors **W**₁, **Z**₁, **U**₁, and **S**₁.

$$O2x := -ZIx - WIx \quad O2x = -0.884$$

$$O2y := -ZIy - WIy \quad O2y = -1.251$$

$$O4x := -SIx - UIx \quad O4x = 3.062$$

$$O4y := -SIy - UIy \quad O4y = -1.251$$

These check with Figure P5-2.

17. Determine the location of the coupler point with respect to point A and line AB.

Distance from A to P $z := \sqrt{ZIx^2 + ZIy^2} \quad z = 2.390 \quad r_p := z$

Angle BAP (δ_p) $s := \sqrt{SIx^2 + SIy^2} \quad s = 2.769$

$$\psi := \text{atan2}(SIx, SIy) \quad \psi = 171.262 \text{ deg}$$

$$\phi := \text{atan2}(Z1x, Z1y) \quad \phi = 99.095 \text{ deg}$$

$$\theta_3 := \text{atan2}(z \cdot \cos(\phi) - s \cdot \cos(\psi), z \cdot \sin(\phi) - s \cdot \sin(\psi))$$

$$\theta_3 = 39.430 \text{ deg}$$

$$\delta_p := \phi - \theta_3 \quad \delta_p = 59.666 \text{ deg}$$

18. DESIGN SUMMARY

Link 1: $g = 3.946$

Link 2: $w = 1.680$

Link 3: $v = 3.054$

Link 4: $u = 0.892$

Coupler point: $r_p = 2.390 \quad \delta_p = 59.666 \text{ deg}$

19. **VERIFICATION:** The calculated values of g (length of the ground link) and of the coordinates of O_2 and O_4 give the same values as those on the problem statement, verifying that the calculated values for the other links and the coupler point are correct.